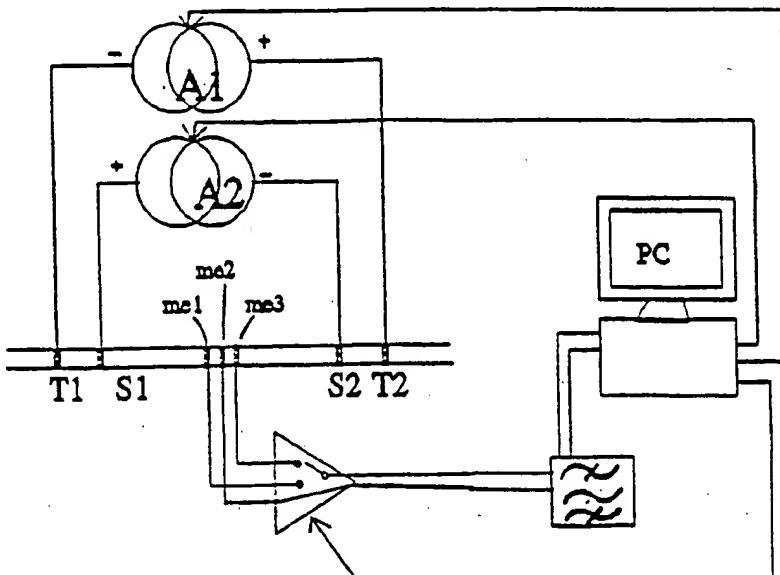




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(54) Title: MEASUREMENT OF ELECTRICAL IMPEDANCE IN BLOOD VESSELS FOR TISSUE IDENTIFICATION USING A MULTI-ELECTRODE CATHETER



(57) Abstract

Method of operating, catheter and catheterization system for measuring electrical impedances in blood vessels within an annular area around the catheter. The catheter contains excitation electrodes (T₁, T₂ & S₁, S₂) between which the impedance is measured, the measurement being a potential difference between measuring electrodes (M_{e1}, M_{e2}, M_{e3}) present between those excitation electrodes. The two pairs of excitation electrodes are electrically driven in opposition to set up a controllable pattern of electric field lines (a so-called "counter current field"). By varying the amplitudes of the two excitation currents, the electric field can be adjusted such that: a) no (or hardly any) current flows between the measuring electrodes (the "quenching relation"), and b) at a distance away from the measuring electrodes the electric field lines are substantially perpendicular to the longitudinal axis of the catheter. The average impedance of the area-to-be-measured and that of the area outside of this given area can then be measured separately.

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MEASUREMENT OF ELECTRICAL IMPEDANCE IN BLOOD VESSELS
FOR TISSUE IDENTIFICATION USING A MULTI-ELECTRODE CATHETER

The invention relates to a method for measuring electrical impedances in blood vessels with the help of a catheter, within an annular area around the catheter, the catheter containing excitation electrodes, which are connected to a current source and the impedance between the electrodes being measured through a potential difference between measuring electrodes, which, apart from the current source are present between those electrodes.

Measuring that electrical impedance is important for the diagnosis of patients with vascular diseases: by means of the value of the impedances along a vessel route affected by constrictions and/or obstructions, it may be possible in combination with data obtained from X-ray photos or ultrasonography to determine the fat content of the material that causes these constrictions and/or obstructions, without the patient being required to undergo surgery. Actually, the specific electrical impedance of fat is much higher than that of blood, vascular tissue, etcetera.

Atherosclerosis is by far the most occurring form of appearance of coarctation in human beings. The importance of information about the fat content in an atherosclerotic lesion is connected with the fact that lesions, rich in fat are less firm of substance than those poor in fat, which makes it easier for them to be torn open, at which a very thrombo-
genic material is released.

Until now it appeared impossible with the existing diagnostic techniques to distinguish in a reliable manner lesions rich in fat over those poor in fat.

Also adaptation of standard impedance catheterization did not lead to the desired result. Impedance catheterization is a method, at which two excitation electrodes are connected to an alternating current source and the circuit is closed because the current can flow to and fro between the electrodes through the environment in which the catheter is located.

Between the excitation electrodes there are two (or more) measuring electrodes. The voltage difference between those measuring electrodes

is a measure for the electrical impedance in the field of current. That this well-known method for measuring impedances did not lead to the intended aim, lies in the fact that one cannot find out whether a change in the impedance takes place near the catheter, in the blood vessel, or 5 farther away, in the tissue next to the blood vessel. Hence conclusions with respect to the blood vessel whether or not being stenosized can not be drawn.

The invention is based on the insight that it is possible to determine changes in the impedance in 'inner area' and 'outer area' separately. 10 The method according to the invention thereto shows the characteristic that two current sources are being used that are connected to two sets of excitation electrodes in such a way and are actuated with such a relation of the respective current intensities that around the catheter a pattern of electrical field lines is generated, a so-called counter current field, at which through variation of the amplitude of the currents of a set of excitation electrodes as regards the other set it will be possible to see to it that between the measuring electrodes no, 15 or hardly any current runs and at a larger distance of the measuring electrodes the electrical field lines are mainly perpendicular to the longitudinal axis of the catheter and that the average impedance of the area to be measured and that of the area outside this will be measured 20 separately, by choosing the relation of the current intensities in such a way that it deviates from the relation at which there is no current between the measuring electrodes, the quenching relation, and by adjusting that relation exactly to that quenching relation respectively. 25

The two current sources are connected and actuated, as it were. 'wrongly', which causes the 'counter current field' to come into existence around the catheter. When such a catheter, adjusted in such a way that there is no or hardly any current flowing between the measuring 30 electrodes, passes a deviating impedance in the small area near the catheter, between the measuring electrodes, that will hardly influence the measured potential difference. At such an counter current field, at which the current fields coming from the two current sources, extinguish each other on the spot of the measuring electrodes, the catheter is fit 35 to detect deviating impedances at a larger distance from the catheter. Said extinguishing is realised at a certain relation - the quenching relation - of the current intensity of the two current-sources. When the

current intensity adjustment starts to deviate from that quenching relation, the electrical field lines pattern becomes more and more such that near the catheter the electrical field lines run approximately parallel to the longitudinal axis of the catheter, so that the influence 5 of deviating impedances in the area near the catheter, between the measuring electrodes becomes relatively larger. By using both the electrical quenching situation and a current source adjustment deviating therefrom that deviation amounting in particular to more than 5% - it will be possible for each position of the catheter in a blood vessel, 10 to determine from the combined measuring data the average impedance for the area outside the blood vessel and the average impedance of the area within the blood vessel - the relevant area in this matter.

Because by adopting the method according to the invention, the division between inner and outer area has been, as it were, 'baked in' 15 in advance, the method is very insensitive to disturbances.

Since the numerical value of the quenching relation, which in a certain situation belongs to the counter current field to be generated, depends on the presence of large deviating impedances near the excitation electrodes, that value can never be exactly predicted. That problem 20 is solved in an embodiment of the method according to the invention by adjusting that relation with the help of a feedback mechanism.

An extra switch is needed for this feedback measuring and it is also important that the measuring electrodes are located very near each other. The impedance catheterization system with which this can be 25 realized thereto shows the characteristic that it contains at least four excitation electrodes that are connected to at least two alternating current sources acting in counterphase, which can be controlled independent from each other and that it is provided with one or more groups of measuring electrodes, which contain per group at least three equidistant electrodes located very close to each other, in such a way that the distance of an arbitrary measuring electrode in a group to a closest other measuring electrode in the same group is the same for all measuring electrodes and smaller than the radius of the blood vessel to be measured, and at which there is no excitation electrode between two 30 measuring electrodes located at said distance from each other.

That system is provided with a preferably digitally controlled switch, with which one may determine between which two measuring elec-

trodes the potential difference is measured.

With the help of the methods described, it will be possible to get a picture of the course of the impedance across the length of the blood vessel to be measured. The catheter is pulled lengthwise through the 5 blood vessel with a speed of preferably not more than 1 cm/sec, each time the impedances being measured in small annular areas located one behind the other within a cylinder around the catheter. Each time when a certain small distance, preferably smaller than the radius of the blood vessel to be measured, has been covered by the catheter, quickly 10 preferably within 10 milliseconds, in a row at least five potential differences are measured: on various pairs of measuring electrodes and at various adjustments of the current sources. From a linear combination of all measuring data thus obtained the impedance in every small annular area around the catheter can be calculated.

15 Preferably the impedance catherization system according to the invention is provided with a digitally controlled switching system, with which one can determine which excitation electrode is connected with which pole of which current source.

In a further preferred embodiment the catherization system according to the invention contains one group of measuring electrodes and is further, in addition to the switch already mentioned, provided with a 20 second switch, with two positions: the counter current position and the parallel position, in the counter current position the two excitation electrodes that are located nearest to the measuring electrodes, being connected to the same current source and in the parallel position are connected to different current sources. In particular such a system contains for instance three measuring electrodes and two current sources and further an electrical device for measuring the potential differences, consisting of one or more 4th class strip guides, signal processors 25 and a AD converter adapter to be installed in a computer, both the operation of the switch that selects two measuring electrodes between which the potential difference is measured, and the operation of the switch with which it is opted for the counter current position or the parallel position, being opered from the same computer, through an DA converter adapter and/or digital I/O adapter.

Good results have been obtained with a distance of the middle measuring electrode to every other measuring electrode of 2 millimetres

and on each side of the middle measuring electrode, while at a distance of 29 millimetres and at a distance of 35 millimetres, a excitation electrode is situated.

In a preferred embodiment of the afore described method, during the movement of the catheter, each time when again a distance equal to the smallest distance between two measuring electrodes has been covered, within 10 milliseconds, the following activities are performed in a row:

- a) determining through arithmetic feedback in particular that current relation between the current sources, to which applies that in the counter current position the potential difference between the first and the second measuring electrode is zero, the measuring electrodes having been numbered onwards, starting with the measuring electrode that is located nearest to the opening where the catheter has been brought into the body;
- b) measuring the potential difference between the second and the third measuring electrode in the counter current position and at the same current intensity relation;
- c) measuring in the parallel position both the potential difference between the first and the second measuring electrode and the potential difference between the second and the third measuring electrode;
- d) adjusting a current intensity relation, which differs more than 5% from the relation as meant sub a) and then measuring both at the parallel position and counter current position both the potential difference between the first and the second measuring electrode and the potential difference between the second and the third measuring electrode.

The invention will be further explained by means of the drawings, in which:

fig.1 schematically shows a known impedance catheter, as it is used for instance to determine the ventricular output of the heart;

fig.2 shows the electrical field lines pattern, belonging to a catheter as shown in fig.1;

fig.3 schematically shows blood vessels respectively without and with impedances influencing the potential difference to be measured;

fig.4 schematically shows an impedance catheterization system according

to the counter current principle;

fig.5 schematically shows the system according to fig.4, but now in the parallel position;

fig.6 shows situations where a catheter is pulled through a blood vessel;

fig.7 shows the catheter with indicated therein numerical values with which a good result has been obtained, and

fig.8 shows in detail a counter current catheterization system according to the invention.

Fig.1 shows schematically a prevailing impedance catheter (a dipole catheter) with two excitation electrodes (S_1 and S_2) and two measuring electrodes (me_1 and me_2). The two excitation electrodes are connected to a current source (A) (alternating current); the circuit is closed because the current can flow from S_1 to S_2 and vice versa through the environment in which the catheter is located. The voltage difference between the measuring electrodes, as read on the voltmeter (V), is a measure for the electrical impedance in the field of current.

Such an impedance catheter is used to determine the ventricular output of the heart. Since blood conducts electrically better than the myocardium and its surroundings, this current difference will fluctuate during the heart cycle: the larger the diameter (and hence the broader the blood column), the lower the impedance and the current difference will be.

The aim with such a catheter is, to create a current field of which the electrical field lines are as parallel as possible to the longitudinal direction (L) of the catheter - see Fig.2: dashed lines with arrows [10] are electrical field lines, the continuous black lines [11] are equipotentials -, so that this results in a relation defined as well as possible between the volume of the ventricle and the measured potential differences. For the accuracy of the measurements it then is favourable to place the measuring electrodes not too close to each other. The better the electrical field lines are parallel to the catheter, the more sensitive the potential difference is to changes in the impedance in the environment of the catheter. In view hereof one uses in some cases extra auxiliary current sources, which through extra excitation electrodes (in addition to said S_1 and S_2) will have the current field run even more homogenously, than is possible with only one current source at a time.

Thus the potential difference measured may give information about the fluctuation of the volume of the ventricle as function of time.

Fig. 3 schematically shows three blood vessel parts 12, 13 and 14, through which a dipole catheter is pulled and of which the impedances are measured. The blood vessel parts 12 and 14 consist of healthy tissue, whereas in part 13 an atherosclerotic lesion (15) of the fat kind is present. The environment of parts 12 and 13 consist of the same material; part 14 runs near a structure with high electrical impedance (for instance bone tissue). The electrical impedance of a fat atherosclerotic lesion is larger than that of blood; this applies, however, also to for instance bone tissue. The potential difference in both part 13 and in part 14 is higher than in part 12. It is hence not possible to conclude from an increased potential difference that a blood vessel shows a fatty lesion: the catheter does not discriminate between the influence of lesion in a blood vessel to the potential difference and that of the impedance outside it.

Fig.4 shows an impedance catherization system according to the counter current principle. It shows two current sources A_1 and A_2 , four excitation electrodes S_1 , S_2 , T_1 and T_2 and a group of three measuring electrodes me_1 , me_2 and me_3 . The amplitude of the current of the current sources A_1 and A_2 can be adjusted; in the drawn case: through a computer and DA converter. The frequencies of the generated alternating currents are the same: for instance 10 kHz and the phase difference between the two alternating currents is 180° ($\pm 0.1^\circ$). This makes it possible to find for a catheter that is located at a place X (seen in the longitudinal direction of the blood vessel), by varying the amplitude of (S_1, S_2) and keeping that of (T_1, T_2) constant, such an adjustment for (S_1, S_2) that the potential difference, measured between the measuring electrodes me_1 and me_2 will equal zero: $\Phi_{11}^1(x) = 0$. This is the earlier mentioned quenching relation: at the spot of the measuring electrodes the two current fields, coming from (S_1, S_2) and (T_1, T_2) respectively, extinguish each other: the 'counter current field'-situation.

Then, while the catheter is still lying motionless and the current source adjustments remain the same, it is possible to measure also the potential difference $\Phi_{11}^1(x)$ between me_2 and me_3 . Whereas at the known dipole catheter the sensitivity is large in the environment of all electrodes, this is different for the measuring of $\Phi_{11}^1(x)$: the area

between the measuring electrodes does not show a high sensitivity and the sensitivity decreases less strongly at an increasing radius (seen from the inside towards the outside) as is the case with the dipole catheter.

5 While the catheter is still lying motionless one may, in order to get a clearly differently shaped sensitivity diagram, equal the amplitude of (S1, S2) to zero (thus a dipole field arises), and then measure $\Phi_{12}^D(x)$ and $\Phi_{23}^D(x)$. In the sensitivity diagram of the measuring of Φ_{23}^D the area between the measuring electrodes is relatively sensitive,

10 The sensitivity diagrams for the measurements of Φ_{23}^D and Φ_{12}^D have in common that the area around the electrodes S1, S2, T1 and T2 is still very sensitive, which makes the difference around the measuring electrodes relatively insignificant. However, realising that if in general one subtracts two measuring signals $\Phi_A - \Phi_B$ from each other, the 15 effective sensitivity diagram belonging to the signal $\Phi_A - \Phi_B$ equals the ('point by point') subtraction of the diagram of Φ_A and that of Φ_B , one may determine the diagrams of $\Phi^I(x) = \Phi_{23}^D(x) - \Phi_{12}^D(x)$ and of $\Phi^D(x) = \Phi_{23}^D(x) - \Phi_{12}^D(x)$.

20 By measuring in this way $\Phi^I(x)$ and $\Phi^D(x)$ the desired separation in inner and outer area for a large part has been 'baked in' already: the value of $\Phi^I(x)$ is mainly determined by the impedances in the outer area; the value of $\Phi^D(x)$ on the contrary is mainly determined by the impedances in the outer area. This makes the result of the final conversion much more reliable.

25 Fig.6 illustrates the situation at which the catheter is moved with a constant speed - along the X axis - in its longitudinal direction: with 16, 17 and 18 three successively occurring situations are shown. At the moment that after departure from situation 16, situation 17 is passed, very quickly $\Phi^I(x + dx)$ and $\Phi^D(x + dx)$ are measured and stored in the PC memory; meanwhile, during the movement from situation 16 to situation 17, upon approaching situation 17 by means of measurements on the measuring electrode set (me1, me2) the amplitude of (S1, S2) has been adjusted such that $\Phi_{12}^I(x + dx) = 0$. Upon approaching situation 18 the same happens, so that $\Phi_{12}^I(x + 2dx) = 0$. At situation 18 $\Phi^I(x + 2dx)$ and $\Phi^D(x + 2dx)$ are measured, etcetera.

30 This is be continued up to and including the Nth situation, at which N can be chosen as large as desired.

The measuring data have now such a structure that by means of a conversion algorithm all x (at short intervals, smaller than the radius of the blood vessel) $R_{outer}(x)$ and $R_{inner}(x)$ can be calculated herefrom.

In the counter current catheterization system according to the invention several times feedback is used in addition to the feedback mentioned to $\Phi_R = 0$. For this purpose the system contains a second digitally controlled switch system with which the current sources can be connected in two ways to the excitation electrodes; this switch systems accordingly knows two positions:

position 1: the 'Counter current position': switching according to figure 4;

position 2: the 'Parallel position': switching according to figure 5.

In the embodiment example of a catheter shown in fig.7, which is used in a counter current catherization system according to the invention the measurements are indicated.

Fig.8 shows more detailed an embodiment example of the counter current catherization system according to the invention, in which [19] is a function generator; [20] is an I/O adapter; [21] are digital attenuators; [22] are current sources with a switch system; [23] is an amplifier with a switch system and [24] is a filter system.

Claims

1. Method for measuring electrical impedances in blood vessels with the help of a catheter, within a annular area around the catheter, the catheter containing excitation electrodes, connected to a current source and the impedance between the electrodes being measured through a potential difference between measuring electrodes which, apart from the current source, are present between those electrodes.

5 characterised in that two current sources are being used that are connected to two sets of excitation electrodes in such a manner and are controlled with such a relation of the respective current intensities,

10 that around the catheter a pattern of electrical field lines arises - a so-called counter current field - at which through variation of the amplitude of the currents of a set of excitation electrodes relation to the other set, one can see to it that between the measuring electrodes no or hardly any current runs and that at a larger distance from the

15 measuring electrodes the electrical field lines are mainly perpendicular to the longitudinal axis of the catheter and that the average impedance of the area to be measured and that of the area outside it, will be measured separately, by choosing the relation of the current intensities such that it deviates from the relation at which there does not run any

20 current between the measuring electrodes - the quenching relation - respectively by adjusting that relation exactly to that quenching relation.

2. Method according to claim 1,

characterised in that for measuring impedances within a blood vessel the relation of the current intensities deviates more than 5% from the quenching relation.

3. Method according to claims 1 or 2,

characterised in that the numerical value of the quenching relation is adjusted with the help of a feedback mechanism.

30 4. Impedance catheter for carrying out the method according to one of the preceding claims, containing excitation electrodes, connected to an alternating current source and with measuring electrodes between which a potential difference can be measured,

characterised in that it contains at least four excitation electrodes that are connected to at least two alternating current sources which are in counterphase, which can be controlled independently from each other;

and that it is provided with one or more groups of measuring electrodes, which contain per group at least three equidistant measuring electrodes, positioned very closely together, such that the distance from one arbitrary measuring electrode in a group, to a nearest other measuring electrode in the same group, for all measuring electrodes is the same and smaller than the radius of the blood vessel to be measured, and situated at said distance from each other between two measuring electrodes, no excitation electrode being present.

5 5. Impedance catheterization system, containing a catheter according to claim 4,

10 characterised in that it is provided with a digitally controlled switch, with which one may determine between which measuring electrodes the potential difference is measured.

15 6. Method according to claims 1 or 2 for obtaining with the help of an impedance catheterization system according to claim 5, a picture of the impedance of small annular areas located in a row in a blood vessel within a cylinder around the catheter, the catheter being pulled lengthwise through a blood vessel and each time when a certain (small) 20 distance has been covered, quickly one after the other at least five potential differences are measured, namely between various pairs of measuring electrodes and at various adjustments of the current sources, such that then from a linear combination of all measuring data thus obtained, the impedance in every annular area around the catheter can be calculated.

25 7. Impedance catheterization system, containing a catheter according to claim 4 and whether or not according to claim 5, characterised in that it is provided with a digitally controlled switch system, with which one may determine which excitation electrode is connected with which pole of which current source.

30 8. Method according to claim 6, a catheter being pulled through the blood vessel at a speed of not more than 1 cm/sec, and the measuring of the potential differences taking place within 10 milliseconds, each time after a movement along a distance that is smaller than the radius of the blood vessel to be measured.

35 9. Impedance catheterization system according to claims 5 or 7, that contains one group of measuring electrodes and that in addition to the switch according to claim 5 is provided with a second switch with

two positions: the counter current position and the parallel position. in the counter current position the two excitation electrodes that are located closest to the measuring electrodes. being connected to the same current source, and in the parallel position are connected to different current sources.

5. 10. Impedance catheterization system according to claim 9, with three measuring electrodes, with two current sources and with an electrical equipment for measuring potential differences, consisting of one or more 4th class strip guides, signal processors and an AD converter adapter to be installed in a computer, both the operation of the switch 10 that selects two measuring electrodes between which the potential difference is measured, and the operation of the switch with which it is opted for the counter current position or the parallel position, being operated from the same computer, through a DA converter adapter and/or 15 digital I/O adapter.

11. Impedance catheterization system according to claim 10, the distance from the middle measuring electrode to every other measuring electrode amounting to 2 millimetres and on each side of the middle measuring electrode, while at a distance of 29 millimetres and at a 20 distance of 35 millimetres an excitation electrode is situated.

12. Method according to claim 8, by means of a catheterization system according to claims 9, 10 or 11, during movement of the catheter, each time when again a distance equal to the smallest distance between 25 two measuring electrodes has been covered, within 10 milliseconds, the following activities being performed in a row:

- a) determining through arithmetic feedback in particular that current relation between the current sources, to which applies that in the counter current position the potential difference between the first and the second measuring electrode is zero, the measuring 30 electrodes having been numbered onwards, starting with the measuring electrode that is located nearest to the opening where the catheter has been brought into the body;
- b) measuring the potential difference between the second and the third measuring electrode in the counter current position and at the same current intensity relation;
- c) measuring in the parallel position both the potential difference

between the first and the second measuring electrode and the potential difference between the second and the third measuring electrode:

- d) adjusting a current intensity relation, which differs more than 5% from the relation as meant sub a) and then measuring both at the parallel position and counter current position both the potential difference between the first and the second measuring electrode and the potential difference between the second and the third measuring electrode.

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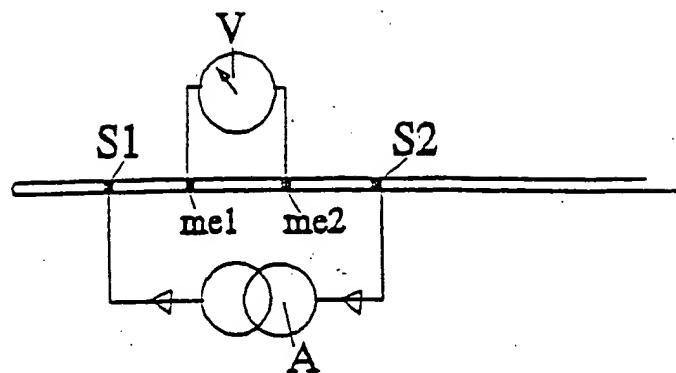


Fig 1

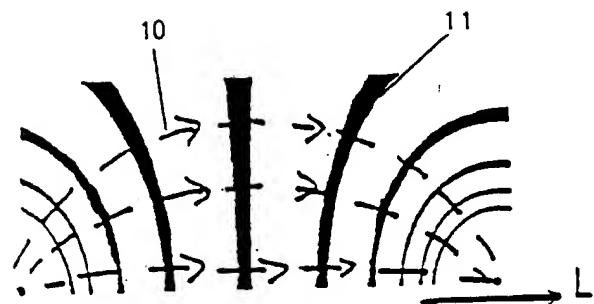


Fig. 2

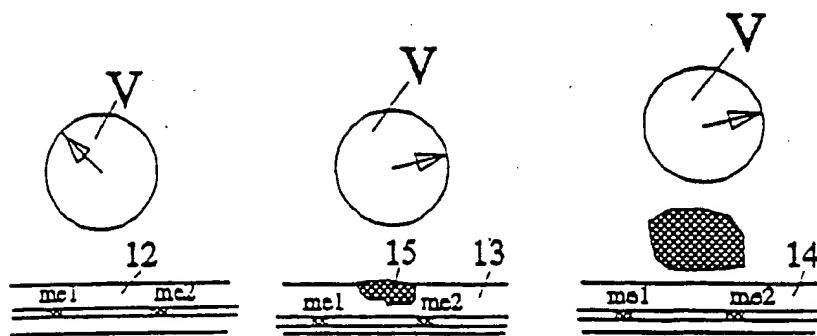


Fig 3

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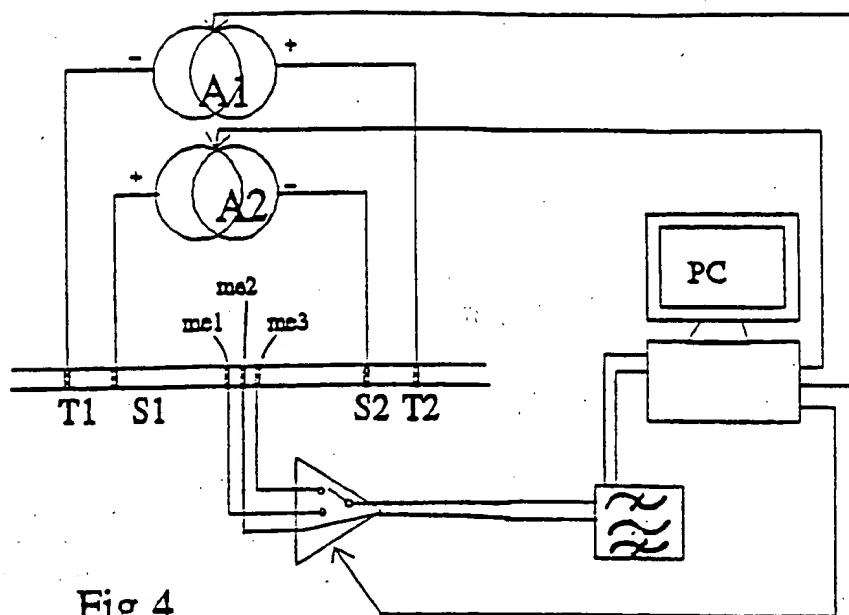


Fig 4

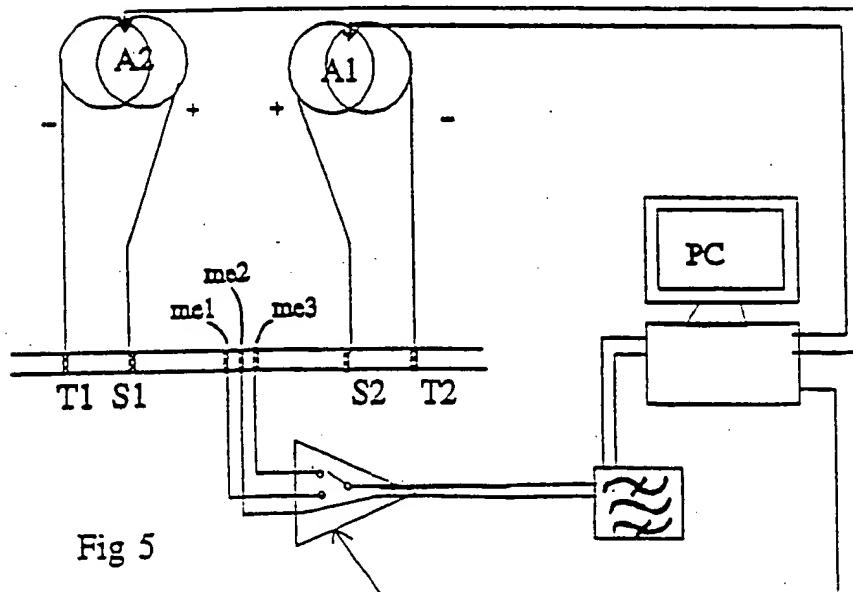


Fig 5

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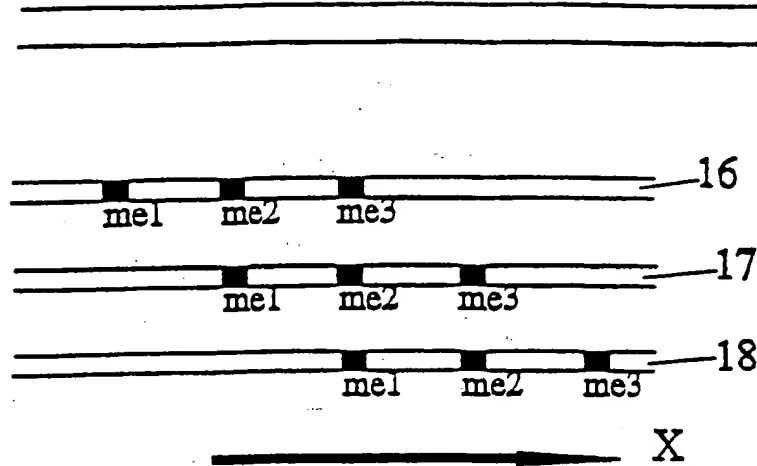


Fig 6

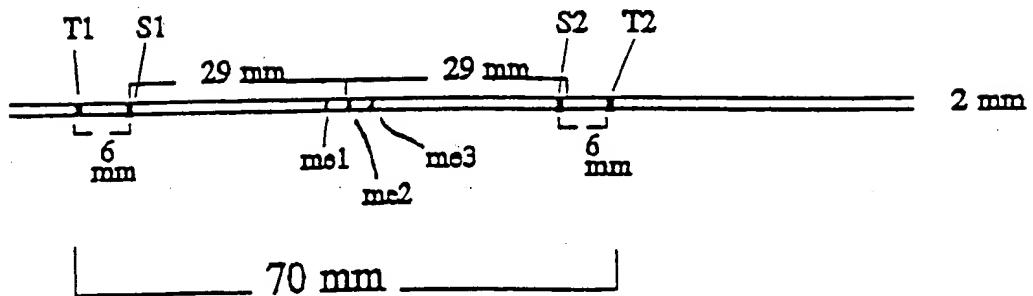
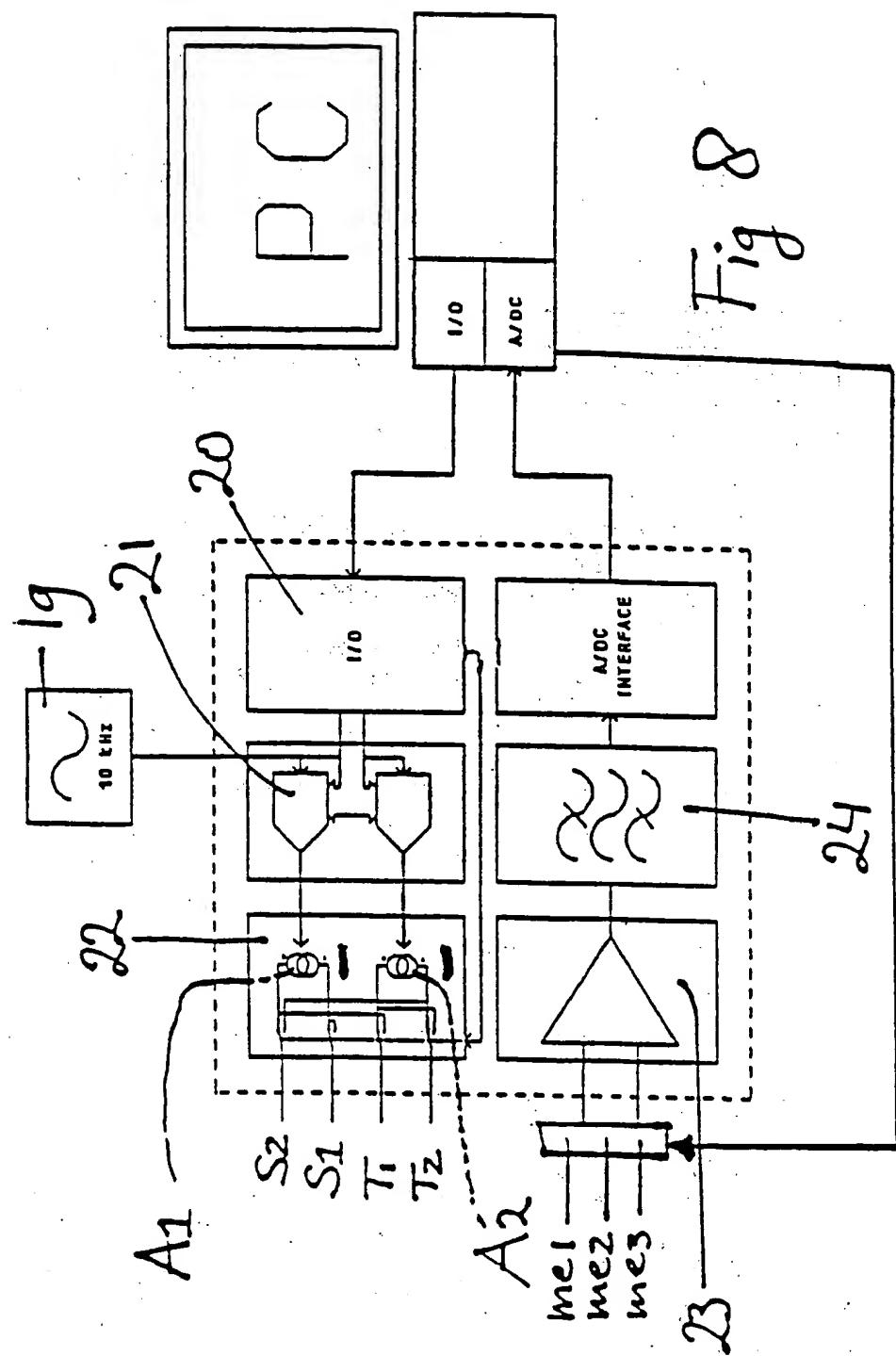


Fig 7



A. CLASSIFICATION OF SUBJECT MATTER
IPC 5 A61B5/05

According to International Patent Classification (IPC) or to both national classification and IPC

B. FIELDS SEARCHED

Minimum documentation searched (classification system followed by classification symbols)
IPC 5 A61B

Documentation searched other than minimum documentation to the extent that such documents are included in the fields searched

Electronic data base consulted during the international search (name of data base and, where practical, search terms used)

C. DOCUMENTS CONSIDERED TO BE RELEVANT

Category	Citation of document, with indication, where appropriate, of the relevant passages	Relevant to claim No.
A	US,A,3 452 743 (R.J.RIEKE) 1 July 1969 see the whole document	1,4,9,12
A	MEDICAL AND BIOLOGICAL ENGINEERING AND COMPUTING., vol.24, no.1, January 1986, STEVENAGE GB pages 62 - 70 N.FURUYA ET AL. 'Development of multielectrode impedance plethysmography' see page 62, paragraph " 2 Instrumentation" ; figure 1	1,4
A	EP,A,0 275 617 (AMERICAN MEDISCAN INC.) 27 July 1988 see abstract; figures 1-6	1,4-7,12
A	US,A,4 852 580 (R.WOOD) 1 August 1989 see the whole document	1
		-/-

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Patent family members are listed in annex.

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Date of the actual completion of the international search

20 May 1994

Date of mailing of the international search report

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